



North Rockwood Developments Inc.

FUNCTIONAL SERVICING AND  
STORMWATER MANAGEMENT REPORT  
5150 WELLINGTON ROAD 27, ROCKWOOD  
TOWNSHIP OF GUELPH-ERAMOSA

**GMBP File No. 318034**  
**Revised January 2020**



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**FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT****NORTH ROCKWOOD DEVELOPMENTS INC.****5150 WELLINGTON ROAD 27, ROCKWOOD****REVISED JANUARY 2020****GMBP FILE NO: 318034**

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**1. INTRODUCTION**

GM BluePlan Engineering Limited has been retained by North Rockwood Developments Inc. to prepare this revised Functional Servicing and Stormwater Management Report in support of a Vacant Land Draft Plan of Condominium application for a residential condominium development located at 5150 Wellington Road 27 in the Township of Guelph-Eramosa (Rockwood) in response to comments received from R.J. Burnside & Associates Limited (dated April 15, 2019).

The subject property, which used to be owned by the Roman Catholic Diocese, is located in the north end of Rockwood, legally described as Part of Lot 7, Concession 4, Geographic Township of Eramosa, Township of Guelph-Eramosa, County of Wellington. Figure No. 1, Site Location Map, shows the location of the proposed development and surrounding area. This report documents the servicing and stormwater management design for this development.

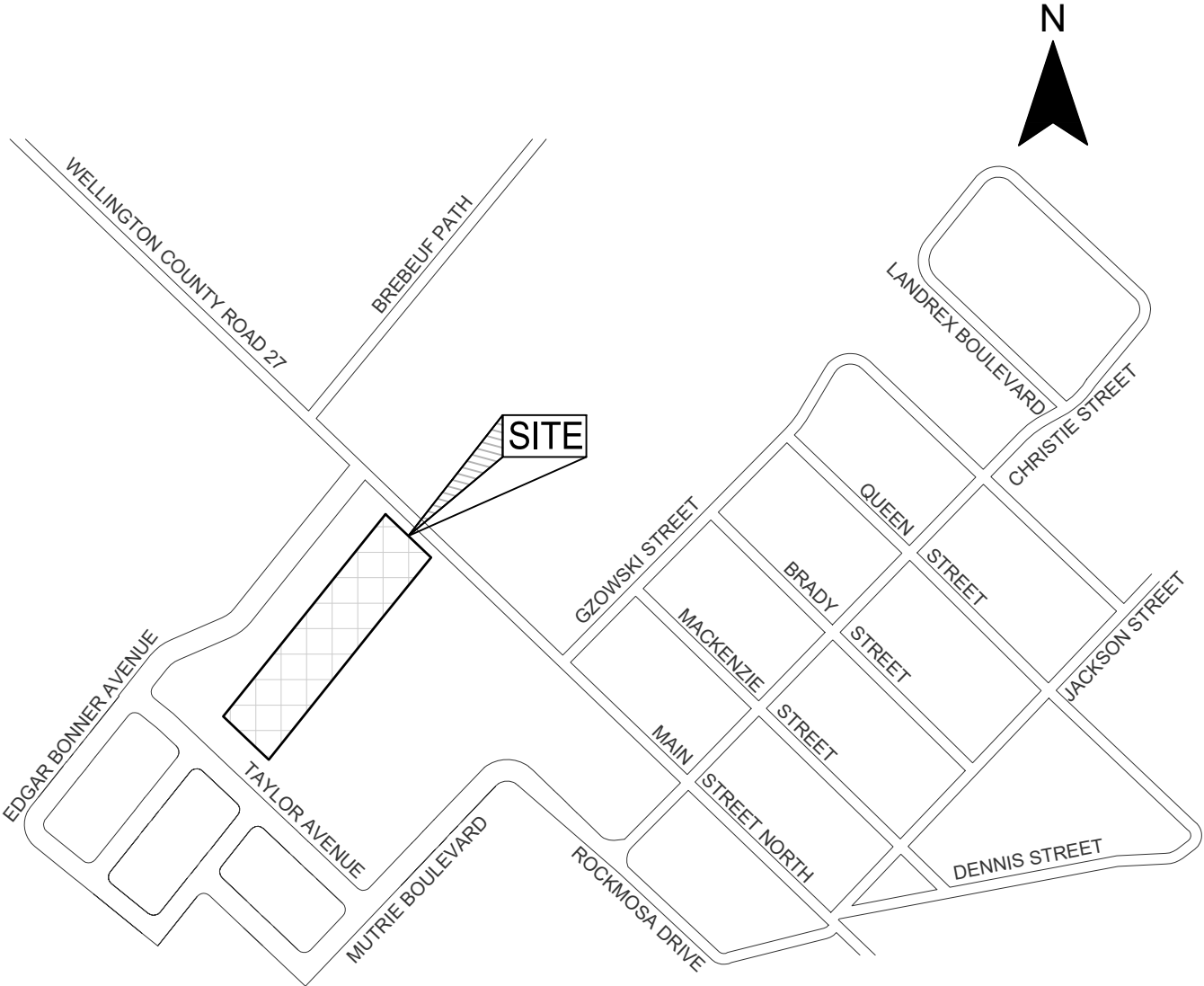
**2. SITE INFORMATION**

The property is currently designated for Residential use in the Wellington County Official Plan and zoned as a Low Density Residential Zone (R1) in Guelph-Eramosa's current Zoning By-Law.

The 1.45-hectare site is situated on the west side of County Road 27 (with approximately 62m frontage), between the Sacred Heart Catholic School (and proposed daycare facility) to the south and the Bonarrow Subdivision to the north and west.

The site is currently a rectangular shaped vacant field gently sloping from the south to the north. Figure No. 2, Existing Conditions Site Plan, shows the existing site conditions, as surveyed by Van Harten Surveying Inc., July 2018.

Functional Servicing and  
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North Rockwood Developments Inc.  
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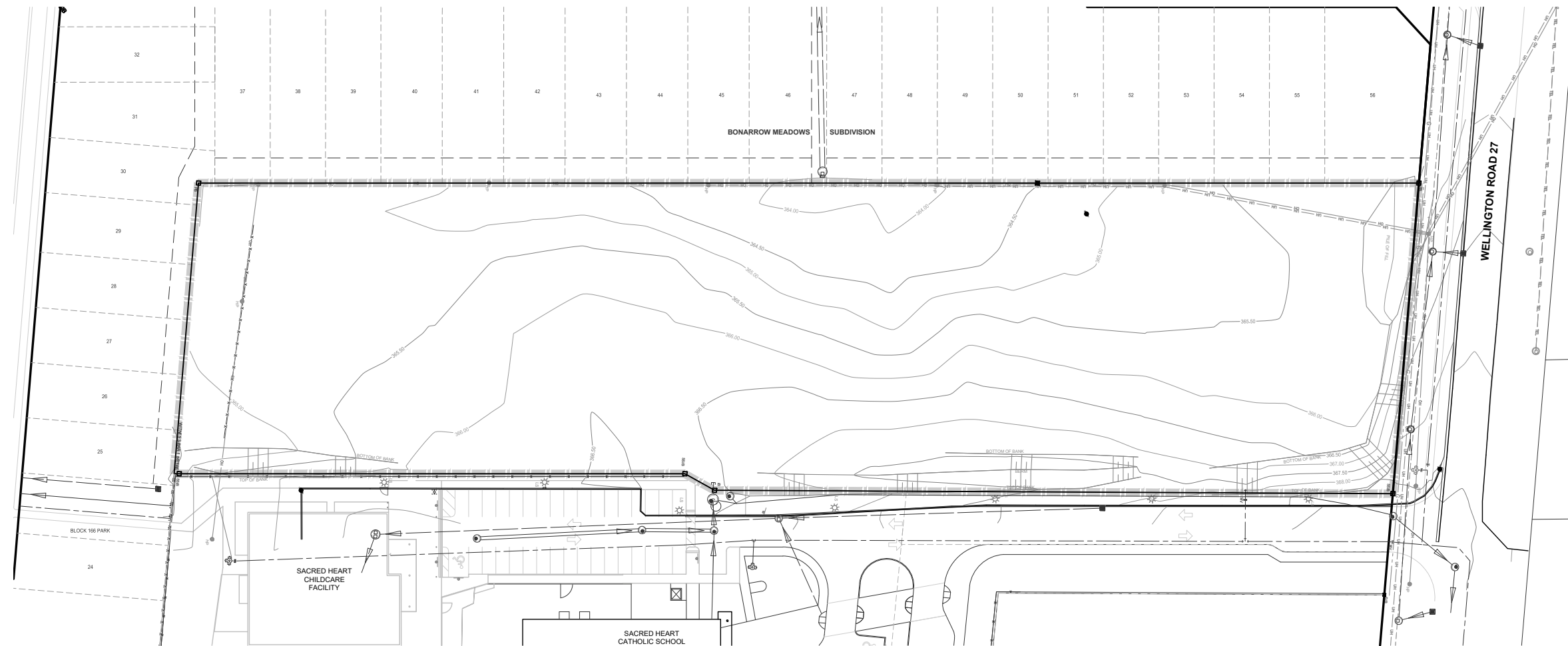
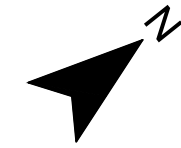
SITE LOCATION MAP

Figure No. 1



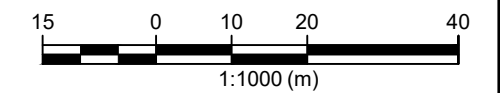
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January 2020  
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Functional Servicing and  
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**LEGEND**

- SITE BOUNDARY
- ORIGINAL TOPOGRAPHICAL CONTOUR



**EXISTING CONDITIONS  
SITE PLAN**

Figure No. 2



### 3. PROPOSED DEVELOPMENT

The proposed plan of condominium has been prepared by Astrid J. Clos Planning Consultants. The plan consists of 51 cluster townhouse dwellings units aligned along an approximately 295m long, 7.0m wide urban common element laneway complete with a turning circle, sidewalk on one side of the street and some other common element areas. (See Figure No.3).

#### 3.1 Grading

Based on our review of the site's topography and our preliminary calculations, the development can be graded to comply with the Township's Development Standards. The site's gentle slope from south to north will provide adequate opportunity for positive drainage with an outlet to the existing 100-year (pre-development) storm outlet, located between units 16 and 17, while providing an emergency overland flow route to the west through the adjacent separate school property and Block 166 of the Bonarrow Subdivision. An agreement to accommodate drainage and servicing through this portion of the adjacent site in an easement has been executed between the Developer and the WCDSB.

Road and lot grades will be designed to ensure proper drainage and sufficient cover over infrastructure. Some storm sewers will require insulation in areas where they will be above the frost penetration depth. Road grades will be constructed at 0.5% to 1.50% for the development. Lot grading will consist of a mixture of lot types such as rear-to-front drainage and split drainage (including walkout and backsplitted lots). Some of the drainage from Lot 32 and the common element area south of the turning circle will be directed to an infiltration gallery. Runoff from roof leaders will be directed to and filtered across grassed surfaces.

During site grading construction, temporary sediment and erosion control measures (such as sediment fencing, sediment ponds, straw bale check dams, etc.) will be implemented for environmental protections. Further details are discussed in Section 7. Figure No. 4, Conceptual Grading Plan, shows the conceptual site grading.

#### 3.2 Sanitary Sewers

A municipal 200mm diameter sanitary sewer currently exists in the Bonarrow Meadows Subdivision, west of the proposed development. The Township has confirmed that there is sufficient reserve capacity in the existing downstream sanitary sewers, sewage pumping station and treatment facility to accommodate this development.

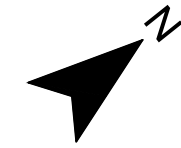
Sanitary service will be provided to the subject property via the extension of a 200mm diameter sanitary sewer to the subject property from the existing 200mm diameter sanitary stub located on Park Block 166 of the Bonarrow Meadows Subdivision, through an easement on the Sacred Heart Catholic School property. The sanitary sewer will then be extended along the length of the proposed internal laneway across the frontage of each unit. Individual 125mm diameter sanitary service lateral connections will be provided for each unit. Figure No. 5, Conceptual Servicing Plan, shows the proposed sanitary sewer servicing layout.

#### 3.3 Watermains

A municipal 200mm diameter watermain currently exists in the Bonarrow Meadows Subdivision, west of the proposed development and on Wellington Road 27, east of the proposed development. A private 200mm diameter watermain also exists along the access road to the Sacred Heart Catholic School. The Township has confirmed that there is sufficient reserve capacity in the existing water system to accommodate this development.

Water service will be provided to the subject property via an extension of a municipal 150mm diameter watermain to the subject property from the existing 200mm diameter watermain stub located on Park Block 166 of the Bonarrow Meadows Subdivision, through a municipal easement on the Sacred Heart Catholic School property, and from the existing 200mm diameter watermain located on Wellington County Road 27 to create a looped system, maximizing redundancy and reliability and minimizing the potential for stagnation. The watermain will then extend along the length of the proposed internal laneway, within a municipal easement, across the frontage of each unit. Individual 25mm diameter water service lateral connections will be provided

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**ASTRID J. CLOS**  
PLANNING CONSULTANTS

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Guelph, Ontario N1H 3X3  
Email: astrid.clos@gplanning.ca  
Phone: (519) 836-7528 (836-PLAN)

**5150 WELLINGTON ROAD 27  
VACANT LAND DRAFT PLAN OF  
CONDOMINIUM**

DATE: DECEMBER 6, 2019 SCALE: 1:500  
PROJECT No. 1916 DRAWN BY: A.R.M.

**KEY MAP**

NOT TO SCALE

**LEGAL DESCRIPTION**  
PART OF LOT 7, CONCESSION 4  
TOWNSHIP OF GUELPH/ERAMOSA (ROCKWOOD)  
COUNTY OF WELLINGTON

**NOTES**

- ALL UNDERGROUND SERVICES INCLUDING WATER SUPPLY LINES REGARDLESS OF LOCATION TO THE EXTENT THE SAME LIE OUTSIDE OF BUILDINGS ARE TO BE COMMON ELEMENTS OF THIS PROPOSED VACANT LAND CONDOMINIUM PLAN.
- THE LOWER VERTICAL LIMIT BOUNDARY OF THAT PART OF A UNIT THAT COMPRISES AN OUTSIDE YARD AREA UNDER WHICH ANY COMMON ELEMENTS WATER LINES SERVICING THE HOMES ARE SITUATE SHALL BE 0.3 OF A METRE BELOW THE UPPER SURFACE OF SUCH YARD AREA. IN ADDITION, THE CONCRETE BASEMENT WALL OF THE HOME APPURTENANT TO ANY SUCH YARD AREAS WILL BE COMMON ELEMENTS TO THE INTERIOR SURFACE OF SUCH BASEMENT CONCRETE WALL.

**LAND USE SCHEDULE**

DESCRIPTION	UNITS	DWELLINGS	AREA (hectares)
CLUSTER TOWNHOUSE	51	51	1.02 ha
COMMON ELEMENT			0.43 ha
	51	51	1.49ha

**ADDITIONAL INFORMATION**  
(UNDER SECTION 5(1) OF THE PLANNING ACT)  
INFORMATION REQUIRED BY CLAUSES 8.3, 8.4, 8.5, 8.6 AND 8.7 ARE AS SHOWN ON THE DRAFT PLAN OF CONDOMINIUM

- n) municipal water
- o) silt/sand
- k) municipal sewer

**OWNER'S CERTIFICATE**  
(AUTHORISE ASTRID J. CLOS, PLANNING CONSULTANTS TO PREPARE AND SUBMIT THIS DRAFT PLAN OF CONDOMINIUM)

\_\_\_\_\_  
CHARL E. NURKEN  
NORTH ROCKWOOD DEVELOPMENTS INC.

\_\_\_\_\_  
FEBRUARY 4, 2019  
DATE

**Van Harten**  
SURVEYING INC.  
LAND SURVEYORS and ENGINEERS

**SURVEYOR'S CERTIFICATE**  
CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED AND THEIR RELATIONSHIP TO THE ADJACENT LANDS ARE CORRECTLY SHOWN.

\_\_\_\_\_  
JAMIE LAWS, O.L.S.  
VAN HARTEN SURVEYING

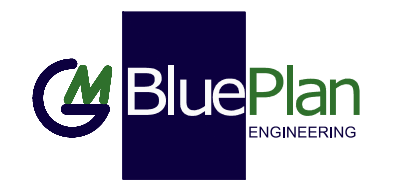
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FEBRUARY 4, 2019  
DATE

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POST DEVELOPMENT  
SITE PLAN  
Figure No. 3







for each unit and hydrants will be spaced as per the Township’s Development Standards. Figure No. 5, Conceptual Servicing Plan, shows the proposed watermain layout.

### 3.4 Storm Sewers

A municipal 675mm diameter storm sewer currently exists in the Bonarrow Meadows Subdivision, north of the proposed development. This storm sewer was sized to convey the 100-year predevelopment flows from the subject property. Other storm sewers in the vicinity of the site include a 250mm diameter storm sewer in Park Block 166 of the Bonarrow Meadows Subdivision and a 375mm diameter storm sewer on Wellington Road 27. The North Pond, an existing municipal stormwater management facility in the Bonarrow Subdivision was designed, approved and constructed with sufficient capacity to accommodate the equivalent of predevelopment flows from this development.

Storm sewers sized to convey and store runoff generated during minor and major storm events will be extended along the proposed internal laneway and through an easement between units 16 and 17, ultimately discharging to the existing 675mm diameter storm sewer and the existing North Pond in the Bonarrow Meadows Subdivision.

## 4. STORMWATER MANAGEMENT

### 4.1 Design Criteria

The stormwater management criteria are as follows:

1. Attenuate the post-development peak flow rates from the site to the existing condition peak flow rates during the 5 and 100-year design storm events.
2. Provide long-term average removal of 80% TSS on an annual basis, prior to discharge from the site.
3. Major storm flows are to be routed overland to an appropriate outlet.
4. Water balance conditions for the site should be managed such that post-development conditions mimic pre-development as much as practically feasible.

The Chicago Storm parameters are provided in Table No. 1 below.

**Table No. 1: Chicago Storm Parameters**

Return Period	A	B	C	Duration (minutes)	Total Depth (mm)
5-Year	539.204	0.093	0.701	180	42.440
100-Year	892.704	0.067	0.704	180	69.184

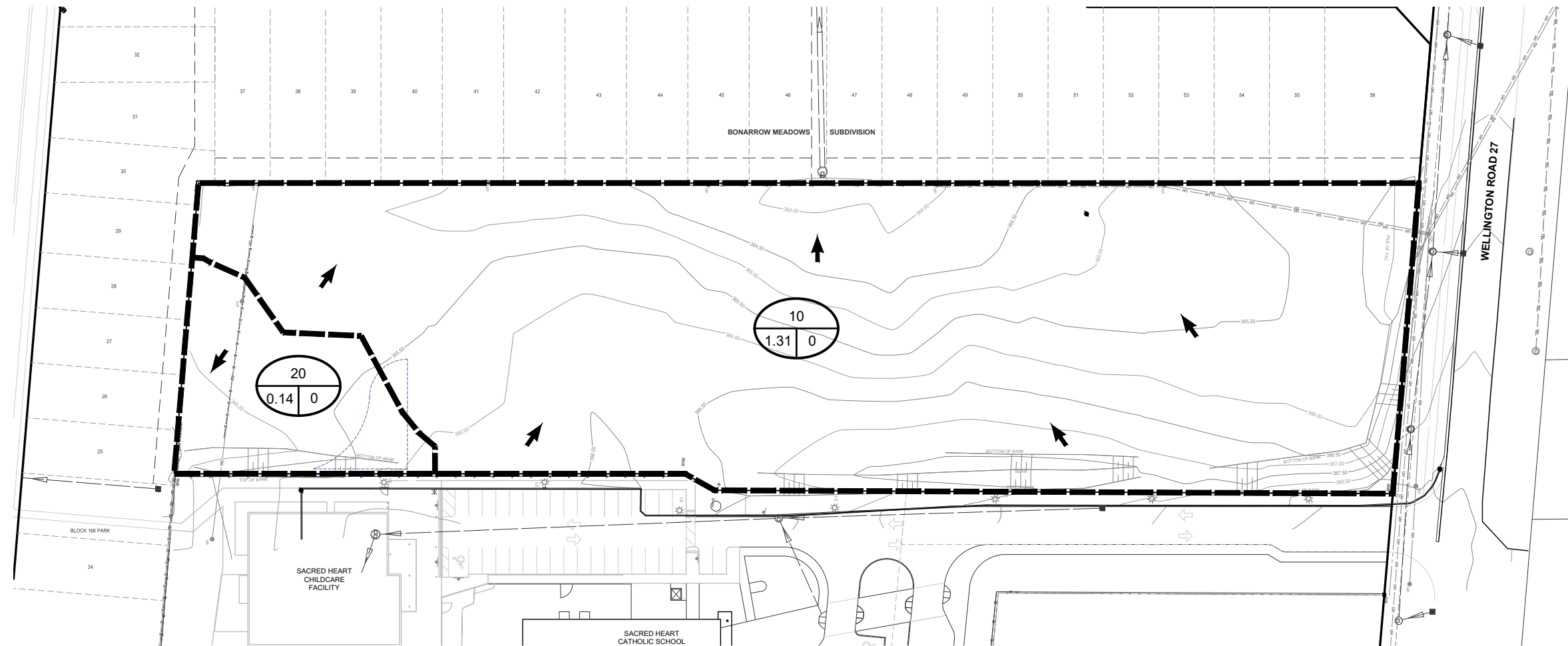
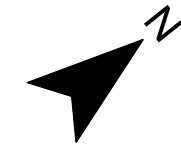
### 4.2 Existing Conditions

For the existing conditions analysis, the 1.45-ha site was modeled as two (2) drainage catchments. The existing conditions drainage catchments are shown on Figure No. 6 and described below. The existing conditions MIDUSS computer modeling is attached in Appendix A.

**Catchment 10 (1.31 hectares, 0% impervious)** represents the majority of the site. Runoff generated from Catchment 10 sheetflows overland to an existing 675mm diameter storm sewer on easement north of the site, ultimately discharging to the existing stormwater management facility (North Pond) on Edgar Bonner Avenue.

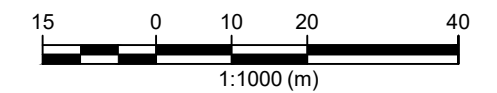
**Catchment 20 (0.14 hectares, 0% impervious)** represents the south corner of the site. Runoff generated from Catchment 20 sheetflows overland to an existing 250mm diameter storm sewer on easement south of the site, ultimately discharging to the existing stormwater management facility (South Pond) on Edgar Bonner Avenue and Mutrie Boulevard.

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**LEGEND**

- DRAINAGE AREA BOUNDARY
- CATCHMENT NUMBER  
% IMPERVIOUS
- CATCHMENT AREA IN HECTARES
- DIRECTION OF SURFACE DRAINAGE



PRE-DEVELOPMENT  
STORM DRAINAGE  
AREA PLAN

Figure No. 6



In summary, the existing condition flow rates from the site are as follows:

**Table No. 2: Existing Condition Flow Rates**

	<b>5-Year</b>	<b>100-Year</b>
Catchment 10	0.088 m <sup>3</sup> /s	0.305 m <sup>3</sup> /s
Catchment 20	0.015 m <sup>3</sup> /s	0.053 m <sup>3</sup> /s
<b>Total</b>	<b>0.101 m<sup>3</sup>/s</b>	<b>0.334 m<sup>3</sup>/s</b>

### 4.3 Allowable Release Rates

The allowable release rates from the site have been established by determining the existing condition flow rates from the site during all storm events.

Therefore, the allowable release rates from the site under post-development conditions are as follows:

**Table No. 3: Allowable Release Rates**

	<b>5-Year</b>	<b>100-Year</b>
Total Flow from Site	0.101 m <sup>3</sup> /s	0.334 m <sup>3</sup> /s

Post-development flow rates generated from the site during the 5 and 100-year design storm events will be attenuated to the allowable release rates.

### 4.4 Post-Development Conditions

For post-development analysis purposes, the site was modeled as four (4) drainage catchments. The post-development drainage catchment is shown on Figure No. 7 and described below. The post-development MIDUSS computer modeling is attached in Appendix A.

**Catchment 100 (0.19 hectares, 50% impervious)** represents the west portion of proposed rooftops and landscaped area that will be conveyed via a grassed swale to the north of the houses, ultimately discharging to the proposed storm sewer on easement and the existing stormwater management facility (North Pond).

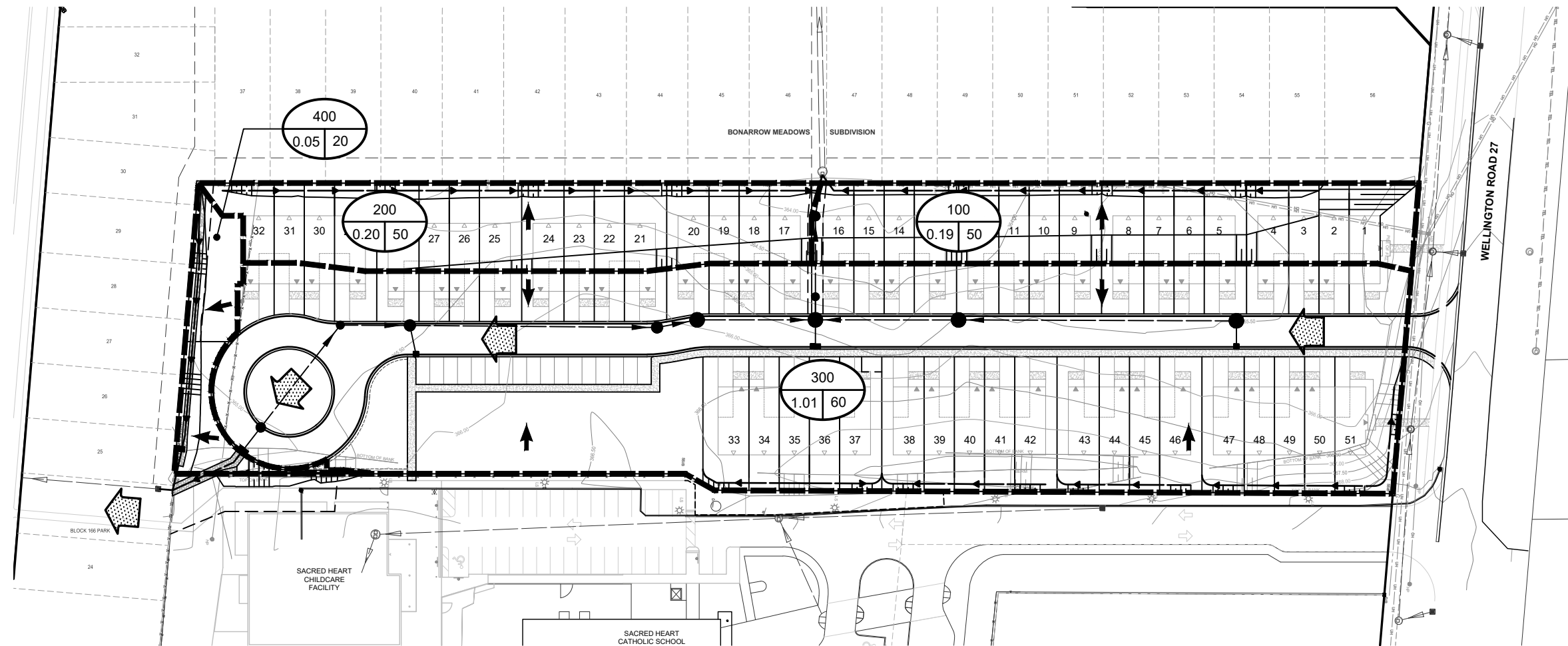
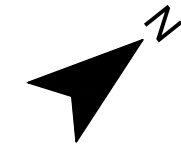
**Catchment 200 (0.20 hectares, 50% impervious)** represents the east portion of proposed rooftops and landscaped area that will be conveyed via a grassed swale to the north of the houses, ultimately discharging to the proposed storm sewer on easement and the existing stormwater management facility (North Pond).

**Catchment 300 (1.01 hectares, 60% impervious)** represents the proposed area that will drain overland to the internal driving aisle. Stormwater runoff generated from Catchment 300 is captured and attenuated on-site via a 450-1200mm diameter super-pipe system consisting of 450 mm diameter, 1050 mm diameter, and 1200 mm diameter storm sewers with approximately 255 m<sup>3</sup> of storage when combined with the storage generated from the storm sewer structures. Stormwater runoff generated from Catchment 300 will ultimately discharge to the existing 675mm diameter storm sewer on easement through the site and to the stormwater management facility (North Pond). Flow which exceeds the capacity of the superpipe system will sheetflow overland south towards Park Block 166 and Taylor Avenue.


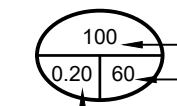


Quality control for stormwater runoff generated from Catchment 300 will be provided via an oil/grit separator structure (Contech CDS PMSU\_2015 or approved equal) prior to discharge to the existing 675mm diameter storm sewer. Details of the oil/grit separator sizing have been included in Appendix A.

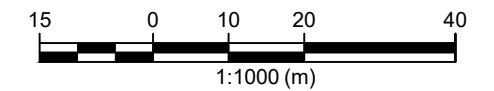
**Catchment 400 (0.05 hectares, 20% impervious)** represents the west portion of proposed rooftop and landscaped area that will be conveyed via a grassed swale to the west of the houses. Runoff generated from Catchment 400 will discharge to the proposed on-site clear stone infiltration gallery in an easement along the west limits of the site. The clear stone infiltration gallery (40m L x 1m W x 1m D) will provide approximately 13.3

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Township of Guelph-Eramosa



**LEGEND**

-  DRAINAGE AREA BOUNDARY
-  CATCHMENT NUMBER  
% IMPERVIOUS  
CATCHMENT AREA IN HECTARES
-  DIRECTION OF SURFACE DRAINAGE
-  DIRECTION OF MAJOR/  
EMERGENCY FLOW ROUTE



POST-DEVELOPMENT  
STORM DRAINAGE  
AREA PLAN

Figure No. 7



m<sup>3</sup> of storage. Flows exceeding the capacity of the clear stone infiltration gallery and grassed swale will sheetflow overland to the catchbasin west of the swale and gallery, ultimately discharging to the proposed storm sewer on easement and the existing stormwater management facility (South Pond).

#### 4.5 Routing

Hydrologic modeling was completed using MIDUSS Version 2.25 using the Horton infiltration method. The stage/storage/discharge relationship for the superpipe system and infiltration gallery is shown in Table No. 4 and Table No. 5 below.

**Table No. 4: Superpipe System Stage/Storage/Discharge Summary**

Control Point	Available Capacities			Actual Capacity Used		
	Peak Flow m <sup>3</sup> /s	Storage Volume m <sup>3</sup>	Storage Depth m	Peak Flow m <sup>3</sup> /s	Storage Volume m <sup>3</sup>	Storage Depth m
Orifice Invert	0.000	0.0	363.25	---	---	---
5-Year	---	---	---	0.034	166.84	364.52
Major Discharge Orifice Invert	0.077	188.22	364.65	---	---	---
100-Year	---	---	---	0.141	241.75	365.24
Top of Grate	0.150	245.27	365.34	---	---	---
Weir	0.162	264.58	365.49	---	---	---
Overflow	0.652	297.57	365.64	---	---	---

**Table No. 5: Infiltration Gallery Stage/Storage/Discharge Summary**

Control Point	Available Capacities			Actual Capacity Used		
	Peak Flow m <sup>3</sup> /s	Storage Volume m <sup>3</sup>	Storage Depth m	Peak Flow m <sup>3</sup> /s	Storage Volume m <sup>3</sup>	Storage Depth m
Bottom of Stone	0.000	0.0	362.45	---	---	---
5-Year	---	---	---	0.001	4.82	362.71
100-Year	---	---	---	0.001	13.01	363.16
Top of Stone	0.001	13.75	363.20	---	---	---
Weir	0.002	14.13	364.25	---	---	---
Overflow	0.050	14.18	364.40	---	---	---

In summary, the post-development flows from the site are as follows:

**Table No. 6: Post-Development Condition Flow Rates**

	<b>5-Year</b>	<b>100-Year</b>
Catchment 100 (uncontrolled)	0.040 m <sup>3</sup> /s	0.077 m <sup>3</sup> /s
Catchment 200 (uncontrolled)	0.042 m <sup>3</sup> /s	0.081 m <sup>3</sup> /s
Catchment 300 (controlled)	0.034 m <sup>3</sup> /s	0.141 m <sup>3</sup> /s
Catchment 400 (controlled)	0.001 m <sup>3</sup> /s	0.001 m <sup>3</sup> /s
<b>Total</b>	<b>0.091 m<sup>3</sup>/s</b>	<b>0.214 m<sup>3</sup>/s</b>

As shown in Table No. 7 below, post-development peak flows have been attenuated to less than the allowable release rates for the 5 and 100-year design storm events.

**Table No. 7: Allowable Release Rates and Post-Development Peak Flow Rates from the Site**

<b>Design Storm</b>	<b>Flow to Edgar Bonner Avenue</b>	
	<b>Allowable Release Rates (m<sup>3</sup>/s)</b>	<b>Post-Development Flows (m<sup>3</sup>/s)</b>
5-Year	0.101 m <sup>3</sup> /s	0.091 m <sup>3</sup> /s
100-Year	0.334 m <sup>3</sup> /s	0.214 m <sup>3</sup> /s

## 4.6 Stormwater Quality

Runoff generated in Catchment 300 will be conveyed to a Contech CDS PMSU\_2025 hydrodynamic separator (or approved equivalent) prior to discharging to the existing 675mm diameter storm sewer on easement. The Contech CDS PMSU\_2025 has been sized such that 80% of the total suspended solids (TSS) are removed. The oil and grit separator design summary is attached as Appendix A.

## 4.7 Water Balance

Per the “Fergus Shand Dam” rainfall station, the average annual precipitation for the area in which the study site is located is estimated to be about 945.7mm. The “Fergus Shand Dam” climate norms were used to estimate an evapotranspiration rate per the Thornthwaite Mather method. It has been estimated that the potential annual evapotranspiration for this area is 586.3 mm for pervious surfaces. Therefore, 359.4 mm remains available for infiltration and runoff. For impervious surfaces within the development, the annual evapotranspiration is estimated to be 192 mm, resulting in approximately 753.7 mm available for infiltration and runoff.

Under post-development conditions, runoff from the west portion of proposed rooftops and landscaped area will be directed to the infiltration gallery on-site. The infiltration gallery has been sized to infiltrate the first 26.7 mm of rainfall. Based on a probability analysis of the “Fergus Shand Dam” rainfall station (2000-2010), the probability of a rainfall event exceeding 26.7 mm is approximately 2.2%. In order to be conservative in our estimate, we will assume that only 95% of the runoff from the rooftop will be infiltrated each year. A similar process was undertaken with each of the infiltration trenches to determine the annual infiltration rates.

From the Geotechnical Investigation completed for the site prepared by Chung & Vander Doelen Engineering Ltd., the native soils in the area of the infiltration gallery were found to be silty gravelly sand and sand and gravel. The sand and gravel can be estimated to naturally infiltrate at a rate of 190mm/year. Additional infiltration

Water Budget - Existing and Post Development Conditions  
 5150 Wellington Road 27  
 Township of Guelph-Eramosa (Rockwood)

	Existing Conditions			Post Development Conditions									Totals		Percent Difference
	10		Existing Total	100		200		300		400		Post-Dev Total	Existing Total	Post-Dev Total	
	Impervious	Pervious		Impervious	Pervious	Impervious	Pervious	Impervious	Pervious	Impervious	Pervious				
Annual Precipitation (mm)	945.7	945.7		945.7	945.7	945.7	945.7	945.7	945.7	945.7	945.7				
Annual Evapotranspiration (mm)	192	586.3		192	586.3	192	586.3	192	586.3	192	586.3				
Available for Recharge & Runoff	753.7	359.4		753.7	359.4	753.7	359.4	753.7	359.4	753.7	359.4				
<b>Total Area (ha)</b>	<b>1.45</b>			<b>0.19</b>		<b>0.20</b>		<b>1.01</b>		<b>0.05</b>					
Area (ha)	0.00	1.45	<b>1.45</b>	0.11	0.08	0.12	0.08	0.61	0.40	0.01	0.04	<b>1.45</b>	<b>1.45</b>	<b>1.45</b>	
Area (m <sup>2</sup> )	0	14,500	<b>14,500</b>	1,140	760	1,200	800	6,060	4,040	100	400	<b>14,500</b>	<b>14,500</b>	<b>14,500</b>	
<b>Annual Infiltration:</b>															
Pervious: @ 190 mm/year	-	2,755	<b>2,755</b>	-	144	-	152	-	768	-	76	<b>1,140</b>	<b>2,755</b>	<b>1,140</b>	
Impervious: @ 0 mm/year	0	-	-	0	-	0	-	0	-	0	-	-	-	-	
Total Annual Infiltration (m <sup>3</sup> /year)	0	2,755	<b>2,755</b>	0	144	0	152	0	768	0	76	<b>1,140</b>	<b>2,755</b>	<b>1,140</b>	
<b>Annual Runoff:</b>															
Pervious: @ 169.4 mm/year	-	2,456	<b>2,456</b>	-	129	-	136	-	684	-	68	<b>1,016</b>	<b>2,456</b>	<b>1,016</b>	
Impervious: @ 753.7 mm/year	0	-	<b>0</b>	859	-	904	-	4,567	-	75	-	<b>6,406</b>	<b>0</b>	<b>6,406</b>	
Total Annual Runoff (m <sup>3</sup> /year)	0	2,456	<b>2,456</b>	859	129	904	136	4,567	684	75	68	<b>7,423</b>	<b>2,456</b>	<b>7,423</b>	
<b>Additional Infiltration:</b>															
Catchment Percent Infiltrated										95%					
Infiltrated m <sup>3</sup> /year										72	64	<b>136</b>	<b>0</b>	<b>136</b>	
<b>Summary:</b>															
Total Runoff (m <sup>3</sup> /year)	0	2,456	<b>2,456</b>	988		1,040		5,252		7		<b>7,287</b>	<b>2,456</b>	<b>7,287</b>	
Total Recharge (m <sup>3</sup> /year)	0	2,755	<b>2,755</b>	144		152		768		212		<b>1,276</b>	<b>2,755</b>	<b>1,276</b>	

occurs when water is captured via an infiltration gallery, allowing a longer retention and drawdown time than overland flow. Following the development, the natural infiltration volume from the site will be 1,102 m<sup>3</sup>/year; the additional infiltration volume from the infiltration gallery will be 136 m<sup>3</sup>/year for a total infiltration volume of 1,276 m<sup>3</sup>/year, leaving an annual runoff volume of 7,287 m<sup>3</sup>/year. The water budget analysis has been completed for the existing and post-development conditions for the site, as included in Appendix 'A'.

## 5. SITE ACCESS AND ROADWAYS

Site access, both vehicular and pedestrian, will be provided from Wellington Road 27. Consistent with current municipal policies and standards, roadways are to be developed to urban standards, including a 6.12m wide carriageway, mountable curb and gutter and sidewalk on one side of the street. Road grades are anticipated to 'seesaw' but will provide an emergency overland outlet for major storm events through the adjacent school site and Block 166 of the Bonarrow Meadows Subdivision. Typical road grades are anticipated to range from 0.5% to 1.50% with a standard road cross fall of 2.0%. A parking area, consisting of 17 standard parking spaces, has been shown at the south end of the site.

The turn circle configuration at the end of the internal roadway, which meets the Ontario Building Code requirements for access route design, with 12.0m dia. centerline radii and mountable curbs, provides sufficient space for fire, waste collection and snow removal trucks to safely turn around. A designated snow storage area is proposed on the north side of the turn circle. If the snow accumulation on site cannot be stored within the designated area it is to be removed from site.

A pedestrian walkway connection is shown between the common element road (behind on the parking spaces) and the future childcare facility on the Sacred Heart School site. The final location and connection of the sidewalk is to be confirmed and negotiated with the Wellington Catholic District School Board.

## 6. UTILITIES AND STREET LIGHTING

Local utility providers include Hydro One Networks, Bell Canada, Cogeco Connexion and Union Gas. All have been contacted for comment regarding the general location and capacity / size of their existing plant at the limits or boundaries of this development and / or the general vicinity, and to provide preliminary comments regarding their desire to service this subdivision and any anticipated opportunities or constraints associated with such servicing.

Hydro One Networks has confirmed that there is currently sufficient capacity in their existing system for this site. They did note that they do not reserve capacity and that it is available on a first come first serve basis. The existing overhead pole line that runs along the north and west lot lines is to be relocated to Wellington Road 27.

Bell Canada expressed interest in servicing this development and indicated that they have existing fiber optic services available near the site. Bell's process for servicing would commence at a later date following Draft plan application, and as detailed design proceeds the Developer's Consultant is to contact Bell and provide plans. At this point, Bell would submit a Greenfield Template to the Bell Governance Board to seek approval. Their decision at that time would be to either serve, to not serve, or to serve with a contribution from the Developer.

Cogeco Connexion has expressed interest in servicing this development and indicated that they have existing aerial plant in the vicinity of the site but may need to construct a small portion of plant to access the site.

Union Gas has expressed interest in servicing this development and indicated that their existing plant, a 100 mm dia. PE 420kPa main, located on the south side of Wellington Road 27 has sufficient capacity.

The Township of Guelph-Eramosa Development Standards include provisions for street lighting on all new internal streets, at the Developer's cost, which would be designed by the Developer's Consultant and coordinated with the Township and Hydro One.

Final confirmation of adequate services and arrangements for utility servicing will be made as the Draft Plan process proceeds, however at this time there does not appear to be any conflicts or restrictions that would significantly delay or prevent the local utilities from servicing the development based on demand.

## 7. SEDIMENT AND EROSION CONTROL

A silt fence will generally be installed along the property boundary and along any environmentally sensitive buffers/areas of the site. The silt fence will serve to minimize the opportunity for water borne sediments to be transported from the site to the adjacent properties. Temporary straw bale check dams will be installed in swales after the initial grading has been completed to slow flow rates and promote the settlement of water borne sediments before they reach the silt fence.

Upon completion of area grading, any area not subject to active construction within an agreed timeframe will be topsoiled and seeded as per OPSS 570 and 572.

Inspection and maintenance of all silt fencing and straw bale check dams will start after installation is complete. The silt fence and check dams will be inspected on a weekly basis during active construction or after a rainfall event of 13 mm or greater. Maintenance will be carried out, within 48 hours, on any part of the features found to need repair.

Once construction has been substantially completed and the ground surface is stabilized, the silt fence and straw bale check dams will be removed, any accumulated sediment within the limits of the development will be collected and removed and the site restoration will be completed.

After construction of the development, erosion and sediment transport will be minimal.

## 8. SOURCE WATER PROTECTION

The proposed site is not located within a Wellhead Protection Area (WHPA) for the Guelph/Eramosa municipal wells, however the WHPAs in Rockwood are being redefined and the site appears to fall into the future WHPA-B with a vulnerability score of 10. This is currently under final review with the Province.

## 9. SUMMARY

In our opinion, the foregoing adequately demonstrates that development of the subject property as an urban residential condominium site with full municipal and utility services is achievable, with no revisions to the Plan of Condominium.

The development will be fully serviced via connections to existing municipal infrastructure (water, sanitary and storm) on existing municipal rights-of-way, blocks or easements. Municipal infrastructure proposed to service the site is accessible and currently has adequate uncommitted reserve capacity in the treatment / supply and collection / distribution systems to accommodate this development.

Associated utility servicing (electrical, tele-communication and natural gas) is also anticipated to be fully achievable.

All of which is respectfully submitted.

GM BLUEPLAN ENGINEERING LIMITED

Per:



Angela Kroetsch, P. Eng.

Encl.



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**Appendix A**  
Stormwater Management Analysis

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```

"                                     Ex_5yr
"                                     ----->"
"      MIDUSS Output ----->"
"      MIDUSS version                      Version 2.25 rev. 473"
"      MIDUSS created                      Sunday, February 07, 2010"
"      10  Units used:                      ie METRIC"
"      Job folder:                        \\gamsby.local\gmprojects>Listowel\2018\
"      318034 5150 wellington Rd 27 Condos Rockwood\5 work in
Progress\Design Data\Modelling Files\2019-01-09"
"      Output filename:                    Ex_5yr.out"
"      Licensee name:                      gmbp"
"      Company                            Hewlett-Packard Company"
"      Date & Time last used:              1/9/2019 at 12:03:52 PM"
" 31      TIME PARAMETERS"
"      5.000  Time Step"
"      180.000 Max. Storm length"
"      1500.000 Max. Hydrograph"
" 32      STORM Chicago storm"
"      1  Chicago storm"
"      539.204 Coefficient A"
"      0.093  Constant B"
"      0.701  Exponent C"
"      0.400  Fraction R"
"      180.000 Duration"
"      1.000  Time step multiplier"
"      Maximum intensity                    172.252  mm/hr"
"      Total depth                          42.440  mm"
"      6  005hyd Hydrograph extension used in this file"
" 33      CATCHMENT 10"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      10  Catchment 10"
"      0.000  % Impervious"
"      1.310  Total Area"
"      100.000 Flow length"
"      5.000  Overland Slope"
"      1.310  Pervious Area"
"      100.000 Pervious length"
"      5.000  Pervious slope"
"      0.000  Impervious Area"
"      100.000 Impervious length"
"      5.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      50.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250  Pervious Lag constant (hours)"
"      5.000  Pervious Depression storage"
"      0.015  Impervious Manning 'n'"
"      0.000  Impervious Max.infiltration"
"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"      0.088  0.000  0.000  0.000 c.m/sec"
"      Catchment 10  Pervious  Impervious Total Area "
"      Surface Area  1.310  0.000  1.310  hectare"
"      Time of concentration  18.940  2.792  18.940  minutes"
"      Time to Centroid  94.453  90.690  94.453  minutes"
"      Rainfall depth  42.440  42.440  42.440  mm"
"      Rainfall volume  555.96  0.00  555.96  c.m"
"      Rainfall losses  32.400  1.928  32.400  mm"
"      Runoff depth  10.040  40.512  10.040  mm"
"      Runoff volume  131.52  0.00  131.52  c.m"
"      Runoff coefficient  0.237  0.000  0.237  "
"      Maximum flow  0.088  0.000  0.088  c.m/sec"

```

```

" 40      HYDROGRAPH Add Runoff "      Ex_5yr
"      4  Add Runoff "
"          0.088      0.088      0.000      0.000"
" 33      CATCHMENT 20"
"      1  Triangular SCS"
"      1  Equal length"
"      2  Horton equation"
"      20  Catchment 20"
"      0.000  % Impervious"
"      0.140  Total Area"
"      20.000  Flow length"
"      2.000  Overland Slope"
"      0.140  Pervious Area"
"      20.000  Pervious length"
"      2.000  Pervious slope"
"      0.000  Impervious Area"
"      20.000  Impervious length"
"      2.000  Impervious slope"
"      0.250  Pervious Manning 'n'"
"      50.000  Pervious Max.infiltration"
"      12.500  Pervious Min.infiltration"
"      0.250  Pervious Lag constant (hours)"
"      5.000  Pervious Depression storage"
"      0.015  Impervious Manning 'n'"
"      0.000  Impervious Max.infiltration"
"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"          0.015      0.088      0.000      0.000 c.m/sec"
"      Catchment 20      Pervious      Impervious      Total Area "
"      Surface Area      0.140      0.000      0.140      hectare"
"      Time of concentration      9.493      1.399      9.493      minutes"
"      Time to Centroid      85.556      88.358      85.556      minutes"
"      Rainfall depth      42.440      42.440      42.440      mm"
"      Rainfall volume      59.42      0.00      59.42      c.m"
"      Rainfall losses      32.461      2.342      32.461      mm"
"      Runoff depth      9.978      40.097      9.978      mm"
"      Runoff volume      13.97      0.00      13.97      c.m"
"      Runoff coefficient      0.235      0.000      0.235      "
"      Maximum flow      0.015      0.000      0.015      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"          0.015      0.101      0.000      0.000"
" 38      START/RE-START TOTALS 20"
"      3  Runoff Totals on EXIT"
"          Total Catchment area      1.450      hectare"
"          Total Impervious area      0.000      hectare"
"          Total % impervious      0.000"
" 38      START/RE-START TOTALS 20"
"      3  Runoff Totals on EXIT"
"          Total Catchment area      1.450      hectare"
"          Total Impervious area      0.000      hectare"
"          Total % impervious      0.000"
" 19      EXIT"

```

```

                                Ex_100yr
"          MIDUSS Output ----->"
"          MIDUSS version                Version 2.25 rev. 473"
"          MIDUSS created                Sunday, February 07, 2010"
"          10 Units used:                ie METRIC"
"          Job folder:                  \\gamsby.local\gmprojects>Listowel\2018\
"          318034 5150 wellington Rd 27 Condos Rockwood\5 work in
Progress\Design Data\Modelling Files\2019-01-09"
"          Output filename:                Ex_100yr.out"
"          Licensee name:                gmbp"
"          Company                      Hewlett-Packard Company"
"          Date & Time last used:        1/9/2019 at 12:02:44 PM"
" 31          TIME PARAMETERS"
"          5.000 Time Step"
"          180.000 Max. Storm length"
"          1500.000 Max. Hydrograph"
" 32          STORM Chicago storm"
"          1 Chicago storm"
"          892.700 Coefficient A"
"          0.067 Constant B"
"          0.704 Exponent C"
"          0.400 Fraction R"
"          180.000 Duration"
"          1.000 Time step multiplier"
"          Maximum intensity            284.814 mm/hr"
"          Total depth                  69.183 mm"
"          6 100hyd Hydrograph extension used in this file"
" 33          CATCHMENT 10"
"          1 Triangular SCS"
"          1 Equal length"
"          2 Horton equation"
"          10 Catchment 10"
"          0.000 % Impervious"
"          1.310 Total Area"
"          100.000 Flow length"
"          5.000 Overland Slope"
"          1.310 Pervious Area"
"          100.000 Pervious length"
"          5.000 Pervious slope"
"          0.000 Impervious Area"
"          100.000 Impervious length"
"          5.000 Impervious slope"
"          0.250 Pervious Manning 'n'"
"          50.000 Pervious Max.infiltration"
"          12.500 Pervious Min.infiltration"
"          0.250 Pervious Lag constant (hours)"
"          5.000 Pervious Depression storage"
"          0.015 Impervious Manning 'n'"
"          0.000 Impervious Max.infiltration"
"          0.000 Impervious Min.infiltration"
"          0.050 Impervious Lag constant (hours)"
"          1.500 Impervious Depression storage"
"          0.305 0.000 0.000 0.000 c.m/sec"
"          Catchment 10 Pervious Impervious Total Area "
"          Surface Area 1.310 0.000 1.310 hectare"
"          Time of concentration 12.992 2.283 12.992 minutes"
"          Time to Centroid 93.500 88.804 93.500 minutes"
"          Rainfall depth 69.183 69.183 69.183 mm"
"          Rainfall volume 906.30 0.00 906.30 c.m"
"          Rainfall losses 40.328 1.995 40.328 mm"
"          Runoff depth 28.855 67.189 28.855 mm"
"          Runoff volume 378.00 0.00 378.00 c.m"
"          Runoff coefficient 0.417 0.000 0.417 "
"          Maximum flow 0.305 0.000 0.305 c.m/sec"

```

```

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"      1  Triangular SCS"
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"      0.000 % Impervious"
"      0.140 Total Area"
"      20.000 Flow length"
"      2.000 Overland Slope"
"      0.140 Pervious Area"
"      20.000 Pervious length"
"      2.000 Pervious slope"
"      0.000 Impervious Area"
"      20.000 Impervious length"
"      2.000 Impervious slope"
"      0.250 Pervious Manning 'n'"
"      50.000 Pervious Max.infiltration"
"      12.500 Pervious Min.infiltration"
"      0.250 Pervious Lag constant (hours)"
"      5.000 Pervious Depression storage"
"      0.015 Impervious Manning 'n'"
"      0.000 Impervious Max.infiltration"
"      0.000 Impervious Min.infiltration"
"      0.050 Impervious Lag constant (hours)"
"      1.500 Impervious Depression storage"
"          0.053      0.305      0.000      0.000 c.m/sec"
"      Catchment 20      Pervious      Impervious      Total Area "
"      Surface Area      0.140      0.000      0.140      hectare"
"      Time of concentration      6.512      1.144      6.512      minutes"
"      Time to Centroid      86.258      86.917      86.258      minutes"
"      Rainfall depth      69.183      69.183      69.183      mm"
"      Rainfall volume      96.86      0.00      96.86      c.m"
"      Rainfall losses      40.594      3.624      40.594      mm"
"      Runoff depth      28.590      65.560      28.590      mm"
"      Runoff volume      40.03      0.00      40.03      c.m"
"      Runoff coefficient      0.413      0.000      0.413      "
"      Maximum flow      0.053      0.000      0.053      c.m/sec"
" 40      HYDROGRAPH Add Runoff "
"      4  Add Runoff "
"          0.053      0.334      0.000      0.000"
" 38      START/RE-START TOTALS 20"
"      3  Runoff Totals on EXIT"
"          Total Catchment area      1.450      hectare"
"          Total Impervious area      0.000      hectare"
"          Total % impervious      0.000"
" 19      EXIT"

```

5150 Wellington Road 27  
 Our File: 318034  
 August 19, 2019

**Catchment 300: Proposed Superpipe Storage**

ELEVATION	DEPTH	SURFACE	PIPE +	INCREASE	ACCUM.	
		PONDING	MANHOLE	STORAGE	STORAGE	
		AREA	STORAGE	VOL	VOL	
(m)	(m)	(m <sup>2</sup> )	VOL	(m <sup>3</sup> )	(m <sup>3</sup> )	
			(m <sup>3</sup> )			
363.25	0.000	0.0	0.00	0.00	0	Pipe Invert
363.45	0.200	0.0	9.58	9.58	9.58	
363.65	0.400	0.0	25.46	25.46	35.04	
363.85	0.600	0.0	26.59	26.59	61.63	
364.05	0.800	0.0	30.86	30.86	92.50	
364.25	1.000	0.0	31.69	31.69	124.19	
364.45	1.200	0.0	31.81	31.81	156.00	Major Discharge Lip
364.65	1.400	0.0	32.22	32.22	188.22	
364.85	1.600	0.0	22.99	22.99	211.21	
365.05	1.800	0.0	22.05	22.05	233.27	
365.25	2.000	0.0	8.89	8.89	242.15	
365.34	2.090	0.0	3.11	3.11	245.27	Top of Grate
365.49	2.240	96.0	4.91	19.31	264.58	Weir
365.64	2.390	279.0	4.87	32.99	297.57	Overflow

**Minor Discharge**

Q = 0.018 m<sup>3</sup>/s  
 Cd = 0.60  
 H = 2.39 m  
 2g = 19.62  
 A = 0.004 m<sup>2</sup>  
 D = 0.075 m

**Major Discharge**

Q = 0.154 m<sup>3</sup>/s  
 Cd = 0.60  
 H = 1.19 m  
 2g = 19.62  
 A = 0.053 m<sup>2</sup>  
 D = 0.260 m

**Weir Calculations**

d1 = 2.39 m  
 h = 2.24 m  
 H = 0.15 m  
 2g = 19.62  
 L = 6.00 m  
 Q = 0.480 m<sup>3</sup>/s

<b>ELEVATION</b>	<b>STORAGE (cu m)</b>	<b>MINOR DISCHARGE (cu m/s)</b>	<b>MAJOR DISCHARGE (cu m/s)</b>	<b>WEIR DISCHARGE (cu m/s)</b>	<b>TOTAL DISCHARGE (cu m/s)</b>	
363.25	0.00	0.0000	0.0000	0.0000	0.0000	Pipe Invert
363.45	9.58	0.0053	0.0000	0.0000	0.0053	
363.65	35.04	0.0074	0.0000	0.0000	0.0074	
363.85	61.63	0.0091	0.0000	0.0000	0.0091	
364.05	92.50	0.0105	0.0000	0.0000	0.0105	
364.25	124.19	0.0117	0.0000	0.0000	0.0117	
364.45	156.00	0.0129	0.0000	0.0000	0.0129	Major Discharge Lip
364.65	188.22	0.0139	0.0631	0.0000	0.0770	
364.85	211.21	0.0149	0.0892	0.0000	0.1041	
365.05	233.27	0.0158	0.1093	0.0000	0.1251	
365.25	242.15	0.0166	0.1262	0.0000	0.1428	
365.34	245.27	0.0170	0.1331	0.0000	0.1501	Top of Grate
365.49	264.58	0.0176	0.1439	0.0000	0.1615	Weir
365.64	297.57	0.0182	0.1539	0.4803	0.6524	Overflow

**5150 Wellington Road 27**  
**Our File: 318034**  
**August 19, 2019**

**Catchment 400: Proposed Infiltration Gallery**

**STORAGE VOLUME CALCULATIONS**

<b>ELEV</b>	<b>INC D</b>	<b>SURFACE AREA (Infil. Gall)</b>	<b>INCR. STORAGE VOL (cu m)</b>	<b>ACCUM STORAGE VOL (cu m)</b>	
<b>(m)</b>	<b>(m)</b>	<b>(sq m)</b>	<b>(cu m)</b>	<b>(cu m)</b>	
362.45	0.000	55.0	0.00	0.00	Bottom of Stone
362.65	0.200	55.0	3.67	3.67	
362.85	0.400	55.0	3.67	7.33	
363.05	0.600	55.0	3.67	11.00	
363.20	0.750	55.0	2.75	13.75	Top of Stone
363.25	0.800	0.36	0.02	13.77	
363.50	1.050	0.36	0.09	13.86	
363.70	1.250	0.36	0.07	13.93	
363.90	1.450	0.36	0.07	14.00	
364.10	1.650	0.36	0.07	14.07	
364.25	1.800	0.36	0.05	14.13	Weir
364.40	1.950	0.36	0.05	14.18	Overflow

**BOTTOM INFILTRATION**

L(dw) =	55.0	m
W(dw) =	1.0	m
D(dw) =	0.75	m
A(c) =	55.0	sq m
VOL(dw)=	41.3	cu m
VOL(st)=	13.8	cu m
K =	22	mm/hr
=	6.11E-04	cm/s

**SIDE INFILTRATION**

**ALL SIDES**

L(dw) =	55.0	m
W(dw) =	1.0	m
D(dw) =	0.75	m
A(c) =	84.0	sq m
K =	22	mm/hr
=	6.11E-04	cm/s

**Weir Calculations**

d1 =	1.95	m
h =	1.80	m
H =	0.15	m
2g =	19.62	
L =	0.60	m
Q =	0.048	m <sup>3</sup> /s

<b>ELEVATION</b>	<b>STAGE</b> <b>(m)</b>	<b>STORAGE</b> <b>(cu m)</b>	<b>INFILTRATION</b> <b>DISCHARGE</b> <b>(cu m/s)</b>	<b>WEIR</b> <b>DISCHARGE</b> <b>(cu m/s)</b>	<b>TOTAL</b> <b>DISCHARGE</b> <b>(cu m/s)</b>	
362.45	0.000	0.00	0.0000	0.0000	0.0000	Bottom of Stone
362.65	0.200	3.67	0.0005	0.0000	0.0005	
362.85	0.400	7.33	0.0006	0.0000	0.0006	
363.05	0.600	11.00	0.0007	0.0000	0.0007	
363.20	0.750	13.75	0.0008	0.0000	0.0008	Top of Stone
363.25	0.800	13.77	0.0009	0.0000	0.0009	
363.50	1.050	13.86	0.0011	0.0000	0.0011	
363.70	1.250	13.93	0.0012	0.0000	0.0012	
363.90	1.450	14.00	0.0013	0.0000	0.0013	
364.10	1.650	14.07	0.0015	0.0000	0.0015	
364.25	1.800	14.13	0.0016	0.0000	0.0016	Weir
364.40	1.950	14.18	0.0017	0.0482	0.0499	Overflow

Post\_\_5yr.out

```

"          MIDUSS Output ----->"
"          MIDUSS version                      Version 2.25  rev. 473"
"          MIDUSS created                      Sunday, February 07, 2010"
"          10  Units used:                      ie METRIC"
"          Job folder:                          W:\Listowel\2018\
"          318034 5150 Wellington Rd 27 Condos Rockwood\5 Work in
Progress\Design Data\Modelling Files\2019-07-31"
"          Output filename:                    Post__5yr.out"
"          Licensee name:                      gmbp"
"          Company                            gmbp"
"          Date & Time last used:              8/1/2019 at 9:24:59 AM"
" 31          TIME PARAMETERS"
"          5.000  Time Step"
"          210.000  Max. Storm length"
"          1500.000  Max. Hydrograph"
" 32          STORM Chicago storm"
"          1  Chicago storm"
"          539.204  Coefficient A"
"          0.093  Constant B"
"          0.701  Exponent C"
"          0.400  Fraction R"
"          180.000  Duration"
"          1.000  Time step multiplier"
"          Maximum intensity                    172.252  mm/hr"
"          Total depth                          42.440  mm"
"          6  005hyd  Hydrograph extension used in this file"
" 33          CATCHMENT 100"
"          1  Triangular SCS"
"          1  Equal length"
"          2  Horton equation"
"          100  Catchment 100"
"          50.000  % Impervious"
"          0.190  Total Area"
"          15.000  Flow length"
"          2.000  Overland Slope"
"          0.095  Pervious Area"
"          15.000  Pervious length"
"          2.000  Pervious slope"
"          0.095  Impervious Area"
"          15.000  Impervious length"
"          2.000  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000  Pervious Max.infiltration"
"          12.500  Pervious Min.infiltration"
"          0.250  Pervious Lag constant (hours)"
"          5.000  Pervious Depression storage"
"          0.015  Impervious Manning 'n'"
"          0.000  Impervious Max.infiltration"

```

Post\_5yr.out

```

"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"              0.040      0.000      0.000      0.000 c.m/sec"
"      Catchment 100      Pervious  Impervious Total Area  "
"      Surface Area      0.095      0.095      0.190      hectare"
"      Time of concentration  8.827      1.177      2.311      minutes"
"      Time to Centroid      83.275      87.989      87.290      minutes"
"      Rainfall depth      42.440      42.440      42.440      mm"
"      Rainfall volume      40.32      40.32      80.64      c.m"
"      Rainfall losses      35.528      2.729      19.128      mm"
"      Runoff depth      6.911      39.711      23.311      mm"
"      Runoff volume      6.57      37.73      44.29      c.m"
"      Runoff coefficient      0.163      0.936      0.549      "
"      Maximum flow      0.008      0.037      0.040      c.m/sec"
" 40      HYDROGRAPH Add Runoff  "
"      4      Add Runoff  "
"              0.040      0.040      0.000      0.000"
" 33      CATCHMENT 200"
"      1      Triangular SCS"
"      1      Equal length"
"      2      Horton equation"
"      200      Catchment 200"
"      50.000      % Impervious"
"      0.200      Total Area"
"      15.000      Flow length"
"      2.000      Overland Slope"
"      0.100      Pervious Area"
"      15.000      Pervious length"
"      2.000      Pervious slope"
"      0.100      Impervious Area"
"      15.000      Impervious length"
"      2.000      Impervious slope"
"      0.250      Pervious Manning 'n'"
"      75.000      Pervious Max.infiltration"
"      12.500      Pervious Min.infiltration"
"      0.250      Pervious Lag constant (hours)"
"      5.000      Pervious Depression storage"
"      0.015      Impervious Manning 'n'"
"      0.000      Impervious Max.infiltration"
"      0.000      Impervious Min.infiltration"
"      0.050      Impervious Lag constant (hours)"
"      1.500      Impervious Depression storage"
"              0.042      0.040      0.000      0.000 c.m/sec"
"      Catchment 200      Pervious  Impervious Total Area  "
"      Surface Area      0.100      0.100      0.200      hectare"
"      Time of concentration  8.827      1.177      2.311      minutes"
"      Time to Centroid      83.275      87.989      87.290      minutes"

```

		Post__5yr.out			
"	Rainfall depth	42.440	42.440	42.440	mm"
"	Rainfall volume	42.44	42.44	84.88	c.m"
"	Rainfall losses	35.528	2.729	19.128	mm"
"	Runoff depth	6.911	39.711	23.311	mm"
"	Runoff volume	6.91	39.71	46.62	c.m"
"	Runoff coefficient	0.163	0.936	0.549	"
"	Maximum flow	0.009	0.038	0.042	c.m/sec"
" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.042	0.081	0.000	0.000"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.042	0.081	0.081	0.000"
" 40	HYDROGRAPH Combine 100"				
"	6 Combine "				
"	100 Node #"				
"	Uncontrolled Flow"				
"	Maximum flow		0.081		c.m/sec"
"	Hydrograph volume		90.913		c.m"
"		0.042	0.081	0.081	0.081"
" 40	HYDROGRAPH Start - New Tributary"				
"	2 Start - New Tributary"				
"		0.042	0.000	0.081	0.081"
" 33	CATCHMENT 300"				
"	1 Triangular SCS"				
"	1 Equal length"				
"	2 Horton equation"				
"	300 Catchment 300"				
"	60.000 % Impervious"				
"	1.010 Total Area"				
"	45.000 Flow length"				
"	2.000 Overland Slope"				
"	0.404 Pervious Area"				
"	45.000 Pervious length"				
"	2.000 Pervious slope"				
"	0.606 Impervious Area"				
"	45.000 Impervious length"				
"	2.000 Impervious slope"				
"	0.250 Pervious Manning 'n'"				
"	75.000 Pervious Max.infiltration"				
"	12.500 Pervious Min.infiltration"				
"	0.250 Pervious Lag constant (hours)"				
"	5.000 Pervious Depression storage"				
"	0.015 Impervious Manning 'n'"				
"	0.000 Impervious Max.infiltration"				
"	0.000 Impervious Min.infiltration"				
"	0.050 Impervious Lag constant (hours)"				
"	1.500 Impervious Depression storage"				

```

                                Post__5yr.out
"          0.207      0.000      0.081      0.081 c.m/sec"
"      Catchment 300      Pervious      Impervious Total Area  "
"      Surface Area      0.404      0.606      1.010      hectare"
"      Time of concentration 17.064      2.276      3.783      minutes"
"      Time to Centroid      90.141      89.764      89.803      minutes"
"      Rainfall depth      42.440      42.440      42.440      mm"
"      Rainfall volume      171.46      257.18      428.64      c.m"
"      Rainfall losses      35.523      1.805      15.292      mm"
"      Runoff depth      6.917      40.635      27.148      mm"
"      Runoff volume      27.94      246.25      274.19      c.m"
"      Runoff coefficient      0.163      0.957      0.640      "
"      Maximum flow      0.023      0.202      0.207      c.m/sec"
" 40      HYDROGRAPH Add Runoff  "
"      4      Add Runoff  "
"          0.207      0.207      0.081      0.081"
" 54      POND DESIGN"
"      0.207      Current peak flow      c.m/sec"
"      0.038      Target outflow      c.m/sec"
"      274.2      Hydrograph volume      c.m"
"      14.      Number of stages"
"      363.250      Minimum water level      metre"
"      365.640      Maximum water level      metre"
"      363.250      Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"      363.250      0.000      0.000"
"      363.450      0.00530      9.580"
"      363.650      0.00740      35.040"
"      363.850      0.00910      61.630"
"      364.050      0.01050      92.500"
"      364.250      0.01170      124.190"
"      364.450      0.01290      156.000"
"      364.650      0.07700      188.220"
"      364.850      0.1041      211.210"
"      365.050      0.1251      233.270"
"      365.250      0.1428      242.150"
"      365.340      0.1501      245.270"
"      365.490      0.1615      264.580"
"      365.640      0.6524      297.570"
"          Peak outflow      0.034      c.m/sec"
"          Maximum level      364.517      metre"
"          Maximum storage      166.839      c.m"
"          Centroidal lag      3.636      hours"
"          0.207      0.207      0.034      0.081 c.m/sec"
" 40      HYDROGRAPH      Combine      100"
"      6      Combine  "
"      100      Node #"
"          Uncontrolled Flow"

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Post__5yr.out
"           Maximum flow           0.091   c.m/sec"
"           Hydrograph volume       365.395   c.m"
"           0.207   0.207   0.034   0.091"
" 40 HYDROGRAPH Start - New Tributary"
"     2 Start - New Tributary"
"           0.207   0.000   0.034   0.091"
" 33 CATCHMENT 400"
"     1 Triangular SCS"
"     1 Equal length"
"     2 Horton equation"
"     400 Catchment 400"
" 20.000 % Impervious"
"     0.050 Total Area"
" 10.000 Flow length"
"     2.000 Overland Slope"
"     0.040 Pervious Area"
" 10.000 Pervious length"
"     2.000 Pervious slope"
"     0.010 Impervious Area"
" 10.000 Impervious length"
"     2.000 Impervious slope"
"     0.250 Pervious Manning 'n'"
" 75.000 Pervious Max.infiltration"
" 12.500 Pervious Min.infiltration"
"     0.250 Pervious Lag constant (hours)"
"     5.000 Pervious Depression storage"
"     0.015 Impervious Manning 'n'"
"     0.000 Impervious Max.infiltration"
"     0.000 Impervious Min.infiltration"
"     0.050 Impervious Lag constant (hours)"
"     1.500 Impervious Depression storage"
"           0.006   0.000   0.034   0.091 c.m/sec"
"           Catchment 400 Pervious Impervious Total Area "
"           Surface Area 0.040 0.010 0.050 hectare"
"           Time of concentration 6.921 0.923 3.373 minutes"
"           Time to Centroid 81.723 87.357 85.056 minutes"
"           Rainfall depth 42.440 42.440 42.440 mm"
"           Rainfall volume 16.98 4.24 21.22 c.m"
"           Rainfall losses 35.678 3.274 29.197 mm"
"           Runoff depth 6.762 39.166 13.243 mm"
"           Runoff volume 2.70 3.92 6.62 c.m"
"           Runoff coefficient 0.159 0.923 0.312 "
"           Maximum flow 0.004 0.004 0.006 c.m/sec"
" 40 HYDROGRAPH Add Runoff "
"     4 Add Runoff "
"           0.006   0.006   0.034   0.091"
" 54 POND DESIGN"
"     0.006 Current peak flow c.m/sec"

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                                Post__5yr.out
"      0.038  Target outflow  c.m/sec"
"      6.6   Hydrograph volume  c.m"
"      12.   Number of stages"
"    362.450  Minimum water level  metre"
"    364.400  Maximum water level  metre"
"    362.450  Starting water level  metre"
"      0     Keep Design Data: 1 = True; 0 = False"
"          Level Discharge  Volume"
"    362.450  0.000  0.000"
"    362.650  0.00050  3.670"
"    362.850  0.00060  7.330"
"    363.050  0.00070  11.000"
"    363.200  0.00080  13.750"
"    363.250  0.00090  13.770"
"    363.500  0.00110  13.860"
"    363.700  0.00120  13.930"
"    363.900  0.00130  14.000"
"    364.100  0.00150  14.070"
"    364.250  0.00160  14.130"
"    364.400  0.04990  14.180"
"          Peak outflow  0.001  c.m/sec"
"          Maximum level  362.713  metre"
"          Maximum storage  4.815  c.m"
"          Centroidal lag  3.571  hours"
"          0.006  0.006  0.001  0.091 c.m/sec"
" 40  HYDROGRAPH  Combine  100"
"      6  Combine "
"    100  Node #"
"          Uncontrolled Flow"
"          Maximum flow  0.091  c.m/sec"
"          Hydrograph volume  372.016  c.m"
"          0.006  0.006  0.001  0.091"
" 38  START/RE-START TOTALS 400"
"      3  Runoff Totals on EXIT"
"          Total Catchment area  1.450  hectare"
"          Total Impervious area  0.811  hectare"
"          Total % impervious  55.931"
" 19  EXIT"

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                                Post__100yr.out
"          MIDUSS Output ----->"
"          MIDUSS version                      Version 2.25  rev. 473"
"          MIDUSS created                      Sunday, February 07, 2010"
"          10  Units used:                      ie METRIC"
"          Job folder:                          W:\Listowel\2018\
"          318034 5150 Wellington Rd 27 Condos Rockwood\5 Work in
Progress\Design Data\Modelling Files\2019-07-31"
"          Output filename:                      Post__100yr.out"
"          Licensee name:                        gmbp"
"          Company                              gmbp"
"          Date & Time last used:                8/1/2019 at 9:27:42 AM"
" 31          TIME PARAMETERS"
"          5.000  Time Step"
"          210.000  Max. Storm length"
"          1500.000  Max. Hydrograph"
" 32          STORM Chicago storm"
"          1  Chicago storm"
"          892.704  Coefficient A"
"          0.067  Constant B"
"          0.704  Exponent C"
"          0.400  Fraction R"
"          180.000  Duration"
"          1.000  Time step multiplier"
"          Maximum intensity                    284.815  mm/hr"
"          Total depth                          69.184  mm"
"          6  100hyd  Hydrograph extension used in this file"
" 33          CATCHMENT 100"
"          1  Triangular SCS"
"          1  Equal length"
"          2  Horton equation"
"          100  Catchment 100"
"          50.000  % Impervious"
"          0.190  Total Area"
"          15.000  Flow length"
"          2.000  Overland Slope"
"          0.095  Pervious Area"
"          15.000  Pervious length"
"          2.000  Pervious slope"
"          0.095  Impervious Area"
"          15.000  Impervious length"
"          2.000  Impervious slope"
"          0.250  Pervious Manning 'n'"
"          75.000  Pervious Max.infiltration"
"          12.500  Pervious Min.infiltration"
"          0.250  Pervious Lag constant (hours)"
"          5.000  Pervious Depression storage"
"          0.015  Impervious Manning 'n'"
"          0.000  Impervious Max.infiltration"

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Post\_100yr.out

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"      0.000  Impervious Min.infiltration"
"      0.050  Impervious Lag constant (hours)"
"      1.500  Impervious Depression storage"
"              0.077      0.000      0.000      0.000 c.m/sec"
"      Catchment 100      Pervious      Impervious      Total Area  "
"      Surface Area      0.095      0.095      0.190      hectare"
"      Time of concentration  5.759      0.963      2.292      minutes"
"      Time to Centroid      84.845      86.466      86.017      minutes"
"      Rainfall depth      69.184      69.184      69.184      mm"
"      Rainfall volume      65.72      65.72      131.45      c.m"
"      Rainfall losses      44.305      4.324      24.315      mm"
"      Runoff depth      24.878      64.859      44.869      mm"
"      Runoff volume      23.63      61.62      85.25      c.m"
"      Runoff coefficient      0.360      0.937      0.649      "
"      Maximum flow      0.032      0.062      0.077      c.m/sec"
" 40      HYDROGRAPH Add Runoff  "
"      4      Add Runoff  "
"              0.077      0.077      0.000      0.000"
" 33      CATCHMENT 200"
"      1      Triangular SCS"
"      1      Equal length"
"      2      Horton equation"
"      200      Catchment 200"
"      50.000      % Impervious"
"      0.200      Total Area"
"      15.000      Flow length"
"      2.000      Overland Slope"
"      0.100      Pervious Area"
"      15.000      Pervious length"
"      2.000      Pervious slope"
"      0.100      Impervious Area"
"      15.000      Impervious length"
"      2.000      Impervious slope"
"      0.250      Pervious Manning 'n'"
"      75.000      Pervious Max.infiltration"
"      12.500      Pervious Min.infiltration"
"      0.250      Pervious Lag constant (hours)"
"      5.000      Pervious Depression storage"
"      0.015      Impervious Manning 'n'"
"      0.000      Impervious Max.infiltration"
"      0.000      Impervious Min.infiltration"
"      0.050      Impervious Lag constant (hours)"
"      1.500      Impervious Depression storage"
"              0.081      0.077      0.000      0.000 c.m/sec"
"      Catchment 200      Pervious      Impervious      Total Area  "
"      Surface Area      0.100      0.100      0.200      hectare"
"      Time of concentration  5.759      0.963      2.292      minutes"
"      Time to Centroid      84.845      86.466      86.017      minutes"

```

Post_100yr.out					
"	Rainfall depth	69.184	69.184	69.184	mm"
"	Rainfall volume	69.18	69.18	138.37	c.m"
"	Rainfall losses	44.305	4.324	24.315	mm"
"	Runoff depth	24.878	64.859	44.869	mm"
"	Runoff volume	24.88	64.86	89.74	c.m"
"	Runoff coefficient	0.360	0.937	0.649	"
"	Maximum flow	0.034	0.065	0.081	c.m/sec"
" 40	HYDROGRAPH Add Runoff "				
"	4 Add Runoff "				
"		0.081	0.157	0.000	0.000"
" 40	HYDROGRAPH Copy to Outflow"				
"	8 Copy to Outflow"				
"		0.081	0.157	0.157	0.000"
" 40	HYDROGRAPH Combine 100"				
"	6 Combine "				
"	100 Node #"				
"	Uncontrolled Flow"				
"	Maximum flow		0.157		c.m/sec"
"	Hydrograph volume		174.988		c.m"
"		0.081	0.157	0.157	0.157"
" 40	HYDROGRAPH Start - New Tributary"				
"	2 Start - New Tributary"				
"		0.081	0.000	0.157	0.157"
" 33	CATCHMENT 300"				
"	1 Triangular SCS"				
"	1 Equal length"				
"	2 Horton equation"				
"	300 Catchment 300"				
"	60.000 % Impervious"				
"	1.010 Total Area"				
"	45.000 Flow length"				
"	2.000 Overland Slope"				
"	0.404 Pervious Area"				
"	45.000 Pervious length"				
"	2.000 Pervious slope"				
"	0.606 Impervious Area"				
"	45.000 Impervious length"				
"	2.000 Impervious slope"				
"	0.250 Pervious Manning 'n'"				
"	75.000 Pervious Max.infiltration"				
"	12.500 Pervious Min.infiltration"				
"	0.250 Pervious Lag constant (hours)"				
"	5.000 Pervious Depression storage"				
"	0.015 Impervious Manning 'n'"				
"	0.000 Impervious Max.infiltration"				
"	0.000 Impervious Min.infiltration"				
"	0.050 Impervious Lag constant (hours)"				
"	1.500 Impervious Depression storage"				

```

                                Post_100yr.out
"          0.381      0.000      0.157      0.157 c.m/sec"
"      Catchment 300      Pervious      Impervious Total Area  "
"      Surface Area      0.404      0.606      1.010      hectare"
"      Time of concentration 11.133      1.862      3.712      minutes"
"      Time to Centroid      90.753      88.160      88.677      minutes"
"      Rainfall depth      69.184      69.184      69.184      mm"
"      Rainfall volume      279.50      419.25      698.75      c.m"
"      Rainfall losses      44.223      2.472      19.172      mm"
"      Runoff depth      24.961      66.712      50.011      mm"
"      Runoff volume      100.84      404.27      505.11      c.m"
"      Runoff coefficient      0.361      0.964      0.723      "
"      Maximum flow      0.084      0.353      0.381      c.m/sec"
" 40      HYDROGRAPH Add Runoff  "
"      4      Add Runoff  "
"          0.381      0.381      0.157      0.157"
" 54      POND DESIGN"
"      0.381      Current peak flow      c.m/sec"
"      0.038      Target outflow      c.m/sec"
"      505.1      Hydrograph volume      c.m"
"      14.      Number of stages"
"      363.250      Minimum water level      metre"
"      365.640      Maximum water level      metre"
"      363.250      Starting water level      metre"
"      0      Keep Design Data: 1 = True; 0 = False"
"          Level Discharge      Volume"
"      363.250      0.000      0.000"
"      363.450      0.00530      9.580"
"      363.650      0.00740      35.040"
"      363.850      0.00910      61.630"
"      364.050      0.01050      92.500"
"      364.250      0.01170      124.190"
"      364.450      0.01290      156.000"
"      364.650      0.07700      188.220"
"      364.850      0.1041      211.210"
"      365.050      0.1251      233.270"
"      365.250      0.1428      242.150"
"      365.340      0.1501      245.270"
"      365.490      0.1615      264.580"
"      365.640      0.6524      297.570"
"          Peak outflow      0.141      c.m/sec"
"          Maximum level      365.241      metre"
"          Maximum storage      241.754      c.m"
"          Centroidal lag      2.831      hours"
"          0.381      0.381      0.141      0.157 c.m/sec"
" 40      HYDROGRAPH      Combine      100"
"      6      Combine  "
"      100      Node #"
"          Uncontrolled Flow"

```

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                                Post__100yr.out
"          Maximum flow                0.214    c.m/sec"
"          Hydrograph volume            682.008    c.m"
"          0.381    0.381    0.141    0.214"
" 40    HYDROGRAPH Start - New Tributary"
"          2    Start - New Tributary"
"          0.381    0.000    0.141    0.214"
" 33    CATCHMENT 400"
"          1    Triangular SCS"
"          1    Equal length"
"          2    Horton equation"
"          400    Catchment 400"
"          20.000    % Impervious"
"          0.050    Total Area"
"          10.000    Flow length"
"          2.000    Overland Slope"
"          0.040    Pervious Area"
"          10.000    Pervious length"
"          2.000    Pervious slope"
"          0.010    Impervious Area"
"          10.000    Impervious length"
"          2.000    Impervious slope"
"          0.250    Pervious Manning 'n'"
"          75.000    Pervious Max.infiltration"
"          12.500    Pervious Min.infiltration"
"          0.250    Pervious Lag constant (hours)"
"          5.000    Pervious Depression storage"
"          0.015    Impervious Manning 'n'"
"          0.000    Impervious Max.infiltration"
"          0.000    Impervious Min.infiltration"
"          0.050    Impervious Lag constant (hours)"
"          1.500    Impervious Depression storage"
"          0.016    0.000    0.141    0.214 c.m/sec"
"          Catchment 400    Pervious    Impervious    Total Area    "
"          Surface Area    0.040    0.010    0.050    hectare"
"          Time of concentration    4.515    0.755    3.035    minutes"
"          Time to Centroid    83.406    86.284    84.539    minutes"
"          Rainfall depth    69.184    69.184    69.184    mm"
"          Rainfall volume    27.67    6.92    34.59    c.m"
"          Rainfall losses    44.425    4.874    36.515    mm"
"          Runoff depth    24.758    64.310    32.669    mm"
"          Runoff volume    9.90    6.43    16.33    c.m"
"          Runoff coefficient    0.358    0.930    0.472    "
"          Maximum flow    0.014    0.007    0.016    c.m/sec"
" 40    HYDROGRAPH Add Runoff "
"          4    Add Runoff "
"          0.016    0.016    0.141    0.214"
" 54    POND DESIGN"
"          0.016    Current peak flow    c.m/sec"

```

```

                                Post_100yr.out
"      0.038  Target outflow    c.m/sec"
"      16.3  Hydrograph volume  c.m"
"      12.   Number of stages"
"    362.450  Minimum water level  metre"
"    364.400  Maximum water level  metre"
"    362.450  Starting water level  metre"
"      0     Keep Design Data: 1 = True; 0 = False"
"          Level Discharge  Volume"
"    362.450    0.000    0.000"
"    362.650    0.00050    3.670"
"    362.850    0.00060    7.330"
"    363.050    0.00070   11.000"
"    363.200    0.00080   13.750"
"    363.250    0.00090   13.770"
"    363.500    0.00110   13.860"
"    363.700    0.00120   13.930"
"    363.900    0.00130   14.000"
"    364.100    0.00150   14.070"
"    364.250    0.00160   14.130"
"    364.400    0.04990   14.180"
"          Peak outflow          0.001    c.m/sec"
"          Maximum level        363.160  metre"
"          Maximum storage       13.013    c.m"
"          Centroidal lag        4.787    hours"
"          0.016    0.016    0.001    0.214 c.m/sec"
" 40    HYDROGRAPH  Combine    100"
"      6    Combine "
"    100    Node #"
"          Uncontrolled Flow"
"          Maximum flow          0.214    c.m/sec"
"          Hydrograph volume     698.350  c.m"
"          0.016    0.016    0.001    0.214"
" 38    START/RE-START TOTALS 400"
"      3    Runoff Totals on EXIT"
"          Total Catchment area          1.450  hectare"
"          Total Impervious area        0.811  hectare"
"          Total % impervious          55.931"
" 19    EXIT"

```



**CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION  
BASED ON THE RATIONAL RAINFALL METHOD  
BASED ON A FINE PARTICLE SIZE DISTRIBUTION**



<b>Project Name:</b> 5150 Wellington Road	<b>Engineer:</b> GM BluePlan Engineering Limited
<b>Location:</b> Rockwood, ON	<b>Contact:</b> Patricia Wiebe, E.I.T
<b>OGS #:</b> 1	<b>Report Date:</b> 18-Jul-19
<b>Area:</b> 1.40 ha	<b>Rainfall Station #:</b> 200
<b>Weighted C:</b> 0.64	<b>Particle Size Distribution:</b> FINE
<b>CDS Model:</b> 2025	<b>CDS Treatment Capacity:</b> 45 l/s

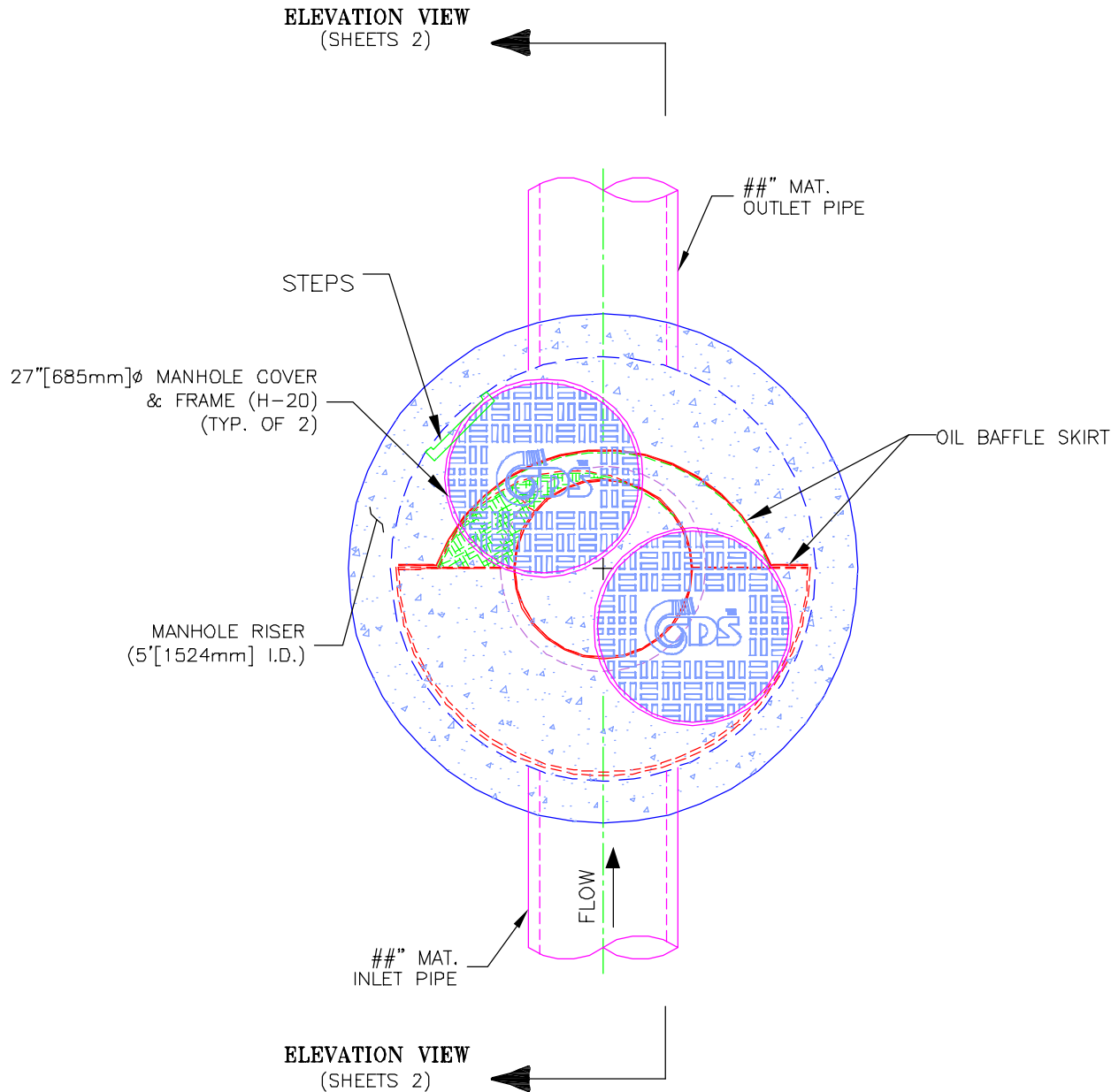
<u>Rainfall Intensity<sup>1</sup></u> <u>(mm/hr)</u>	<u>Percent Rainfall Volume<sup>1</sup></u>	<u>Cumulative Rainfall Volume</u>	<u>Total Flowrate (l/s)</u>	<u>Treated Flowrate (l/s)</u>	<u>Operating Rate (%)</u>	<u>Removal Efficiency (%)</u>	<u>Incremental Removal (%)</u>
1.0	9.7%	18.2%	2.5	2.5	5.5	97.3	9.5
1.5	8.5%	26.7%	3.7	3.7	8.2	96.5	8.2
2.0	8.2%	34.9%	5.0	5.0	11.0	95.7	7.8
2.5	6.2%	41.1%	6.2	6.2	13.7	94.9	5.9
3.0	6.3%	47.4%	7.5	7.5	16.5	94.1	5.9
3.5	3.9%	51.3%	8.7	8.7	19.2	93.3	3.6
4.0	4.0%	55.3%	10.0	10.0	22.0	92.6	3.7
4.5	4.0%	59.3%	11.2	11.2	24.7	91.8	3.7
5.0	3.5%	62.8%	12.5	12.5	27.5	91.0	3.2
6.0	6.4%	69.2%	14.9	14.9	33.0	89.4	5.8
7.0	4.7%	74.0%	17.4	17.4	38.5	87.8	4.2
8.0	3.4%	77.4%	19.9	19.9	44.0	86.3	2.9
9.0	2.6%	79.9%	22.4	22.4	49.5	84.7	2.2
10.0	1.9%	81.9%	24.9	24.9	55.0	83.1	1.6
15.0	9.1%	90.9%	37.4	37.4	82.5	75.2	6.8
20.0	3.8%	94.7%	49.8	45.3	100.0	63.8	2.4
25.0	2.7%	97.5%	62.3	45.3	100.0	51.1	1.4
30.0	0.7%	98.1%	74.7	45.3	100.0	42.6	0.3
35.0	0.8%	98.9%	87.2	45.3	100.0	36.5	0.3
40.0	0.5%	99.4%	99.6	45.3	100.0	31.9	0.1
45.0	0.3%	99.6%	112.1	45.3	100.0	28.4	0.1
50.0	0.0%	99.6%	124.5	45.3	100.0	25.5	0.0
							87.9

Removal Efficiency Adjustment<sup>2</sup> = 6.5%  
**Predicted Net Annual Load Removal Efficiency = 81.4%**  
**Predicted Annual Rainfall Treated = 96.8%**

1 - Based on 34 years of hourly rainfall data from Canadian Station 6149387, Waterloo ON  
 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.  
 3 - CDS Efficiency based on testing conducted at the University of Central Florida  
 4 - CDS design flowrate and scaling based on standard manufacturer model & product specifications



# PLAN VIEW



## CDS MODEL PMSU20\_25m, 1.7 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME  
CITY, STATE

JOB# XX-##-###

DATE ##/##/##

DRAWN INITIALS

APPROV.

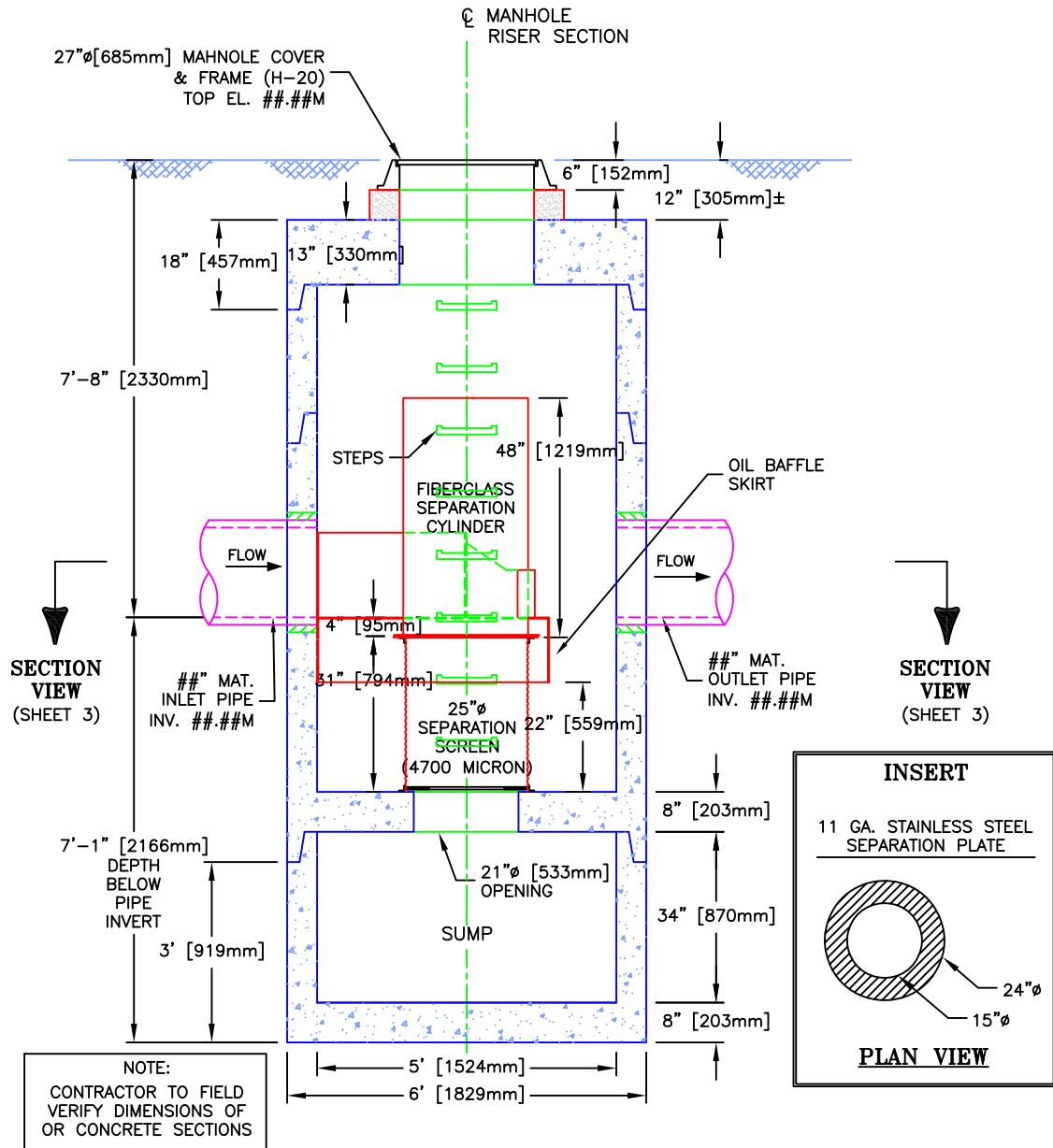
SCALE  
1" = 2'

SHEET

1



# ELEVATION VIEW



## CDS MODEL PMSU20\_25m, 1.7 CFS TREATMENT CAPACITY STORM WATER TREATMENT UNIT



PROJECT NAME  
CITY, STATE

JOB# XX-##-###

DATE ##/##/##

DRAWN INITIALS

APPROV.

SCALE  
1" = 3'

SHEET

2